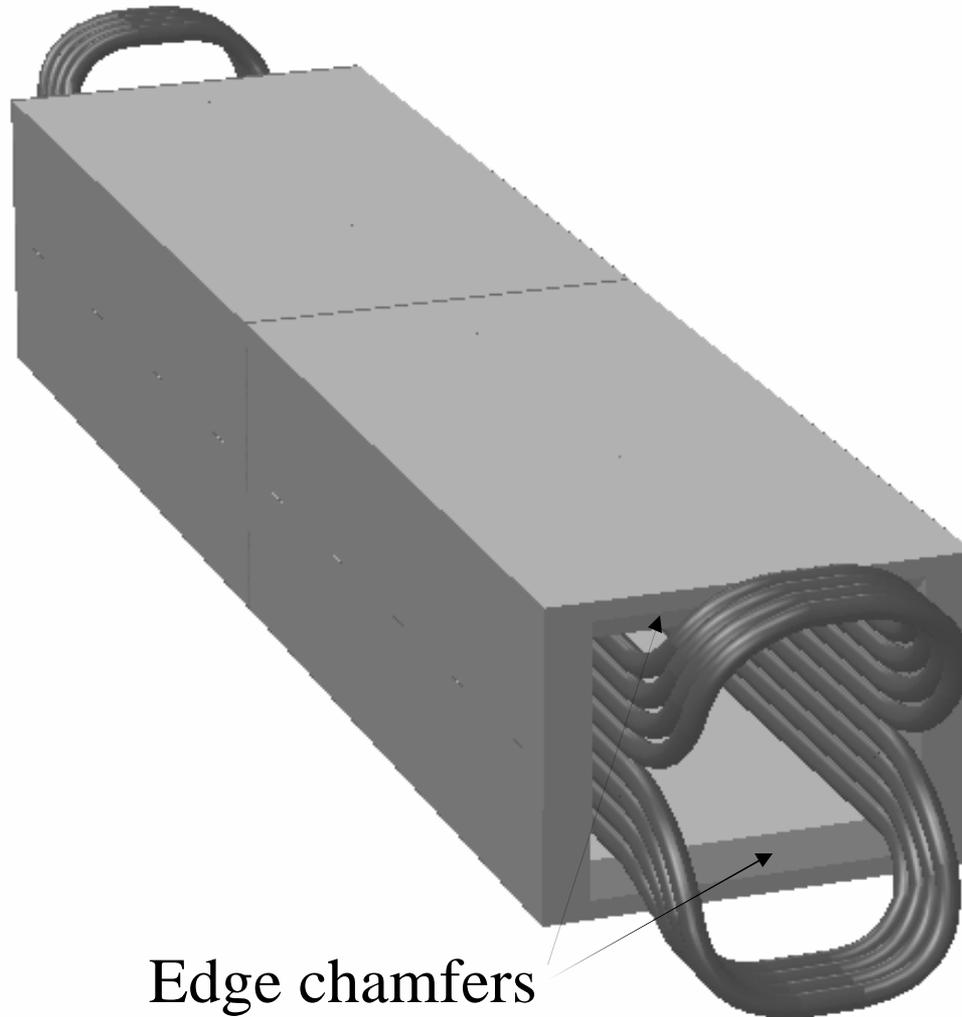


# Optimization

W. Meng (4/2/2008)

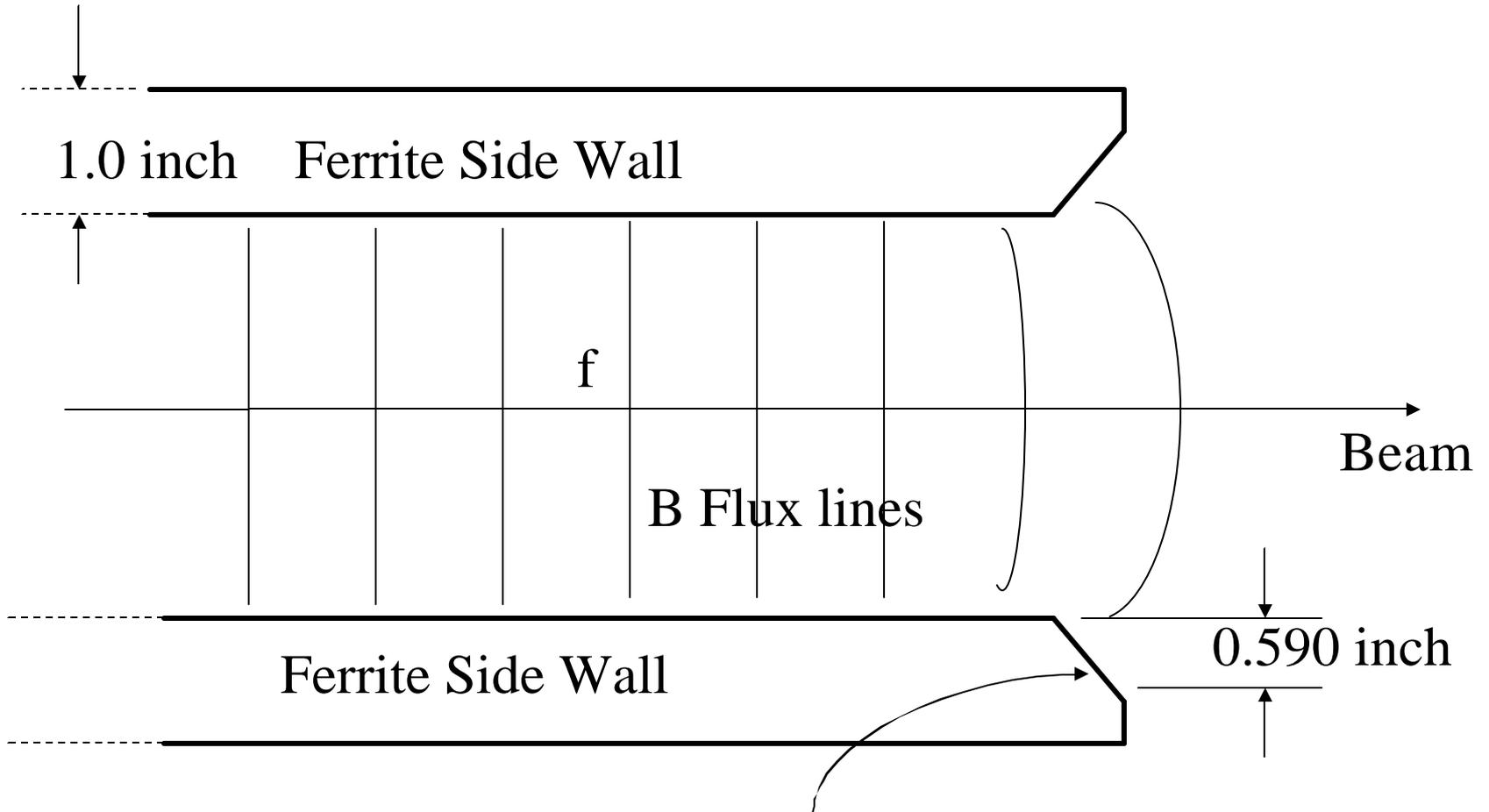
- (1) Based on the selected New England Litz Wire geometry:  
d=0.5 inch, with round cross-section
  - (2) Based on the real winding end crossing configuration  
from 3d engineering design of the coil mandrels
  - (3) Edge chamfers (on ferrite core) are applied and optimized  
to minimize the integrated first allowed high order  
component b<sub>3</sub> (6-pole)
- ( 3d simulations up to December 2007 were done by  
using simplified 8-turn square cross-section “saddle coils”.)

## 3d View – coil-end and edge chamfers



Edge chamfers

# Top view (assuming field in horizontal direction)



Four (4) Edge chamfers (45 degree) per magnet, should be machined on four (4) longer-side of window inner edges.

## Final(?) Parameters (calculated)

Current:  $I_0 = 118.58$  A --- amplitude of  $I = I_0 \cdot \sin(2\pi ft)$

Central field:  $B_0 = 99.085$  Gauss

Integrated dipole field = 100.58 Gauss-meter

Dipole magnetic (or effective) length = 1.015 meter

Ratio of integrated 6-pole to dipole  $< 1E-4$  (@ $R=2$  cm)

Stored magnetic energy = 0.6433 Joule (per magnet at peak)

Self-inductance =  $9.150E-5$  H = 91.50  $\mu$ H (per magnet)

Note:

Ferrite (cmd5005) thickness (1.0 inch), length (0.92 m), and window size (0.12 x 0.176 m) remain unchanged. Additional machined edge chamfers (0.590x0.590 inch) are required.