

CORRECTION

I said yesterday that ceramic coating of conductor pipe is not broken up to 1mm/m bending...

It is not exactly.

I have not bended a ceramic-coated pipe until broken.

I saw that a 7.5mm*7.5mm hollow conductor of copper ceramic-coated was self-weighted down to about 1mm/m, perhaps, more. And it is not broken.

I do not know the limit.

But I think that ceramic coating is more flexible.

Design of DC-Septum magnets of the injection and extraction system of the Rapid Cycle Synchrotron(RCS) for the J-PARC

14th ICFA mini-workshop on septa devices

平成17年3月1日
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Member of designing of RCS's septa

日本原子力研究所(JAERI)
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CONTENS

- INTRODUCTION

- DESIGN

- PROTOTYPE

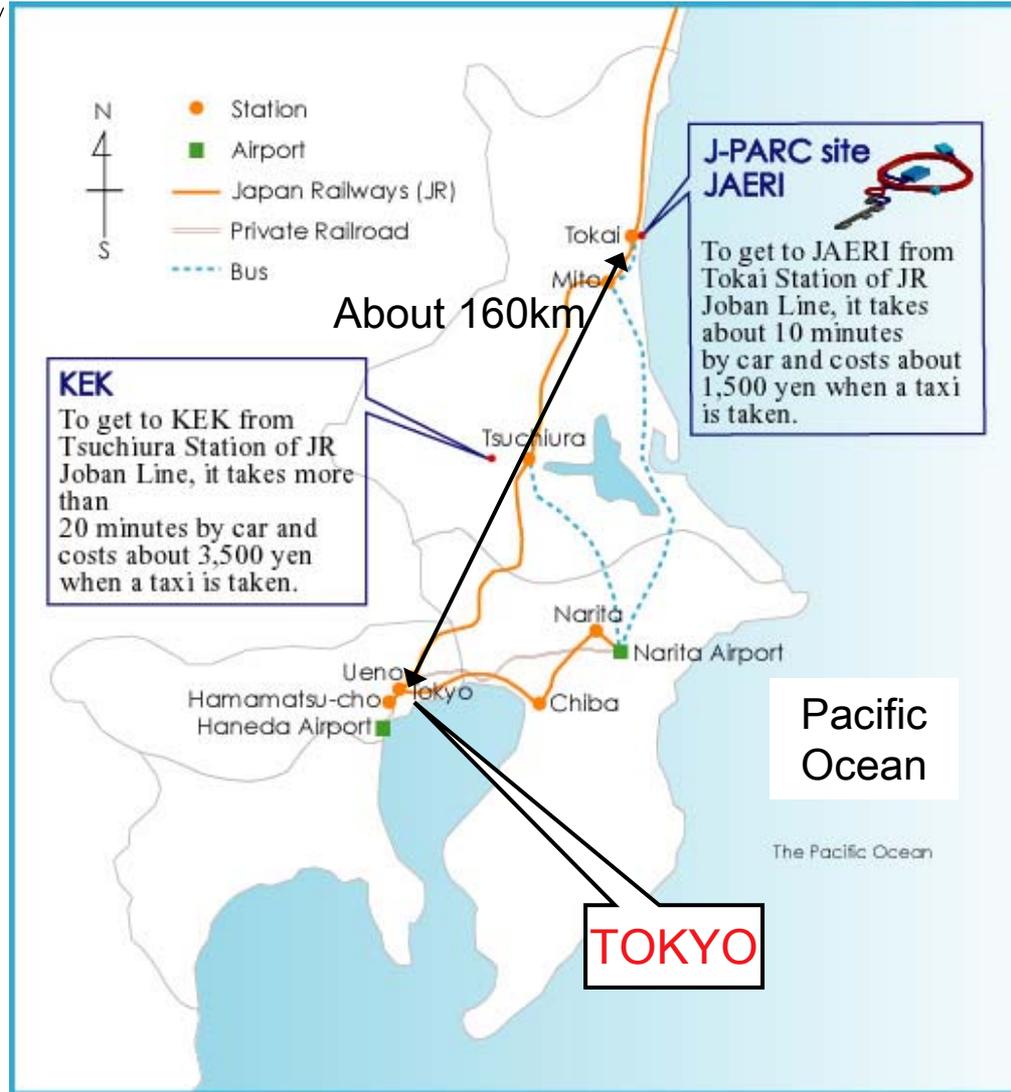
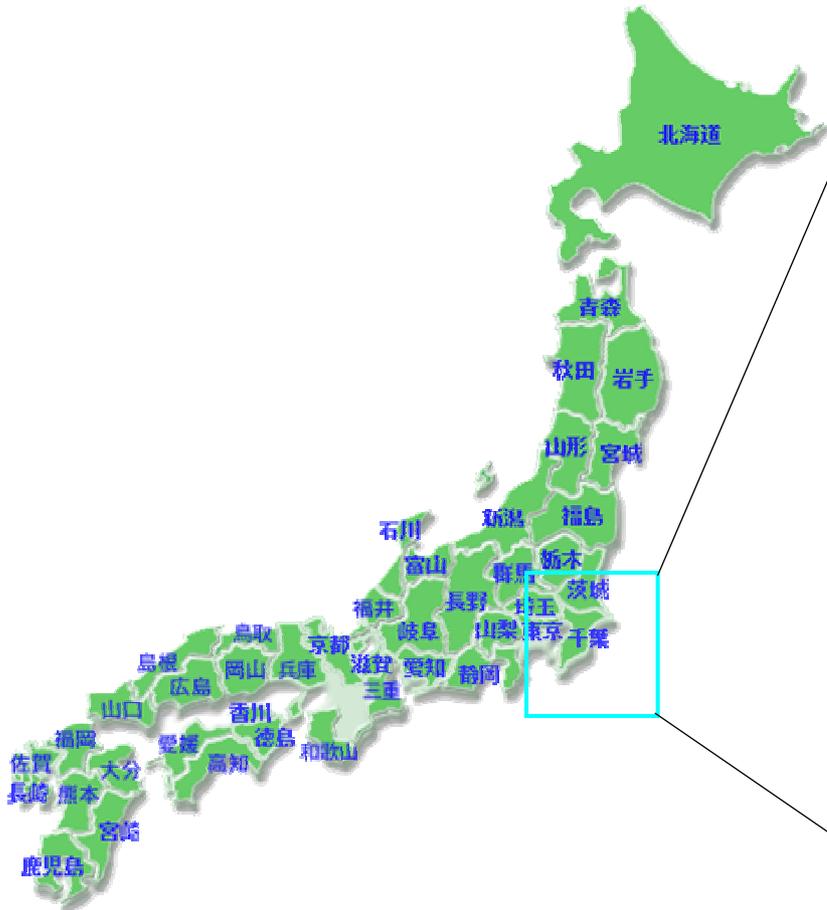
- Concept of coil support and insulation

J-PARC <http://jkj.tokai.jaeri.go.jp/index.html>

JAERI and KEK Joint Project

Japan Proton Accelerator Research Complex
High Intensity Accelerator Project

JAERI...Japan Atomic Energy Research Institute
KEK..Ko Enerugi kasokuki Kenkyu kiko



KEK
To get to KEK from Tsuchiura Station of JR Joban Line, it takes more than 20 minutes by car and costs about 3,500 yen when a taxi is taken.

J-PARC site JAERI
To get to JAERI from Tokai Station of JR Joban Line, it takes about 10 minutes by car and costs about 1,500 yen when a taxi is taken.

About 160km

TOKYO

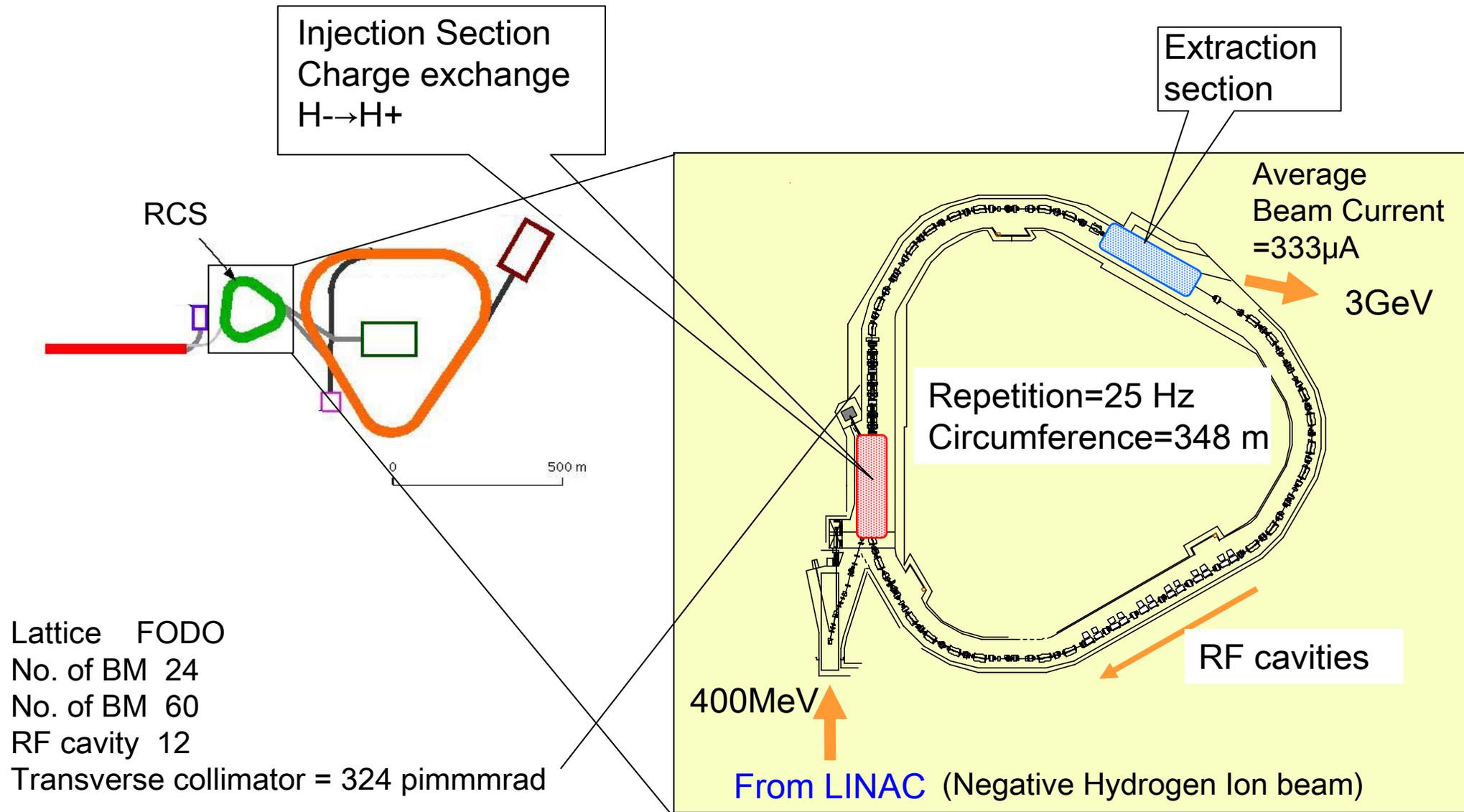
Pacific Ocean

The Pacific Ocean

PLAN of J-PARC



RCS Rapid Cycle Synchrotron



INJECTION system

High Intensity Machine → Multi-turn Injection (to fill phase space)

Charge Exchange Injection ← Liouville theorem

Charge exchange foils (electron stripper, H→H⁺) and 4 bump magnets

Phase Space Painting ← Space Charge Effect

horizontal painting ...to move ring orbit using 4 bump magnets in the RCS ring

vertical painting ...to move injection line using pulse magnets in the BT line

Conceptual design by **Dr.SAKAI**

Main charge exchange foil, carbon

Fail in e- stripping

start of painting

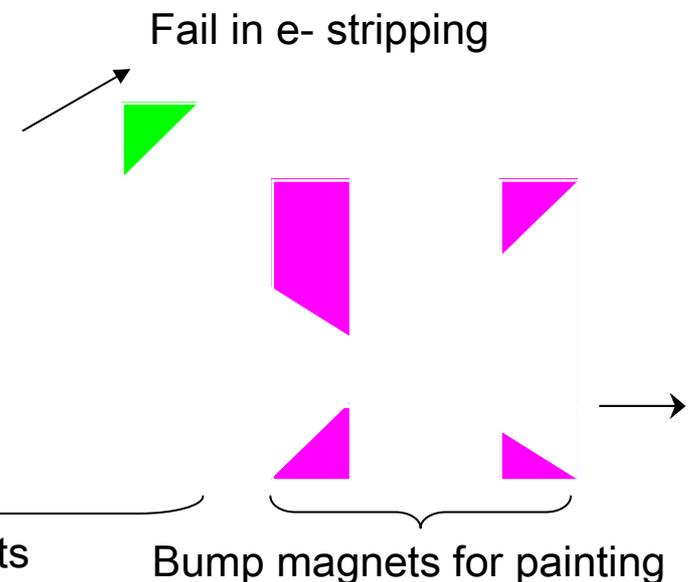
end of painting

Ring

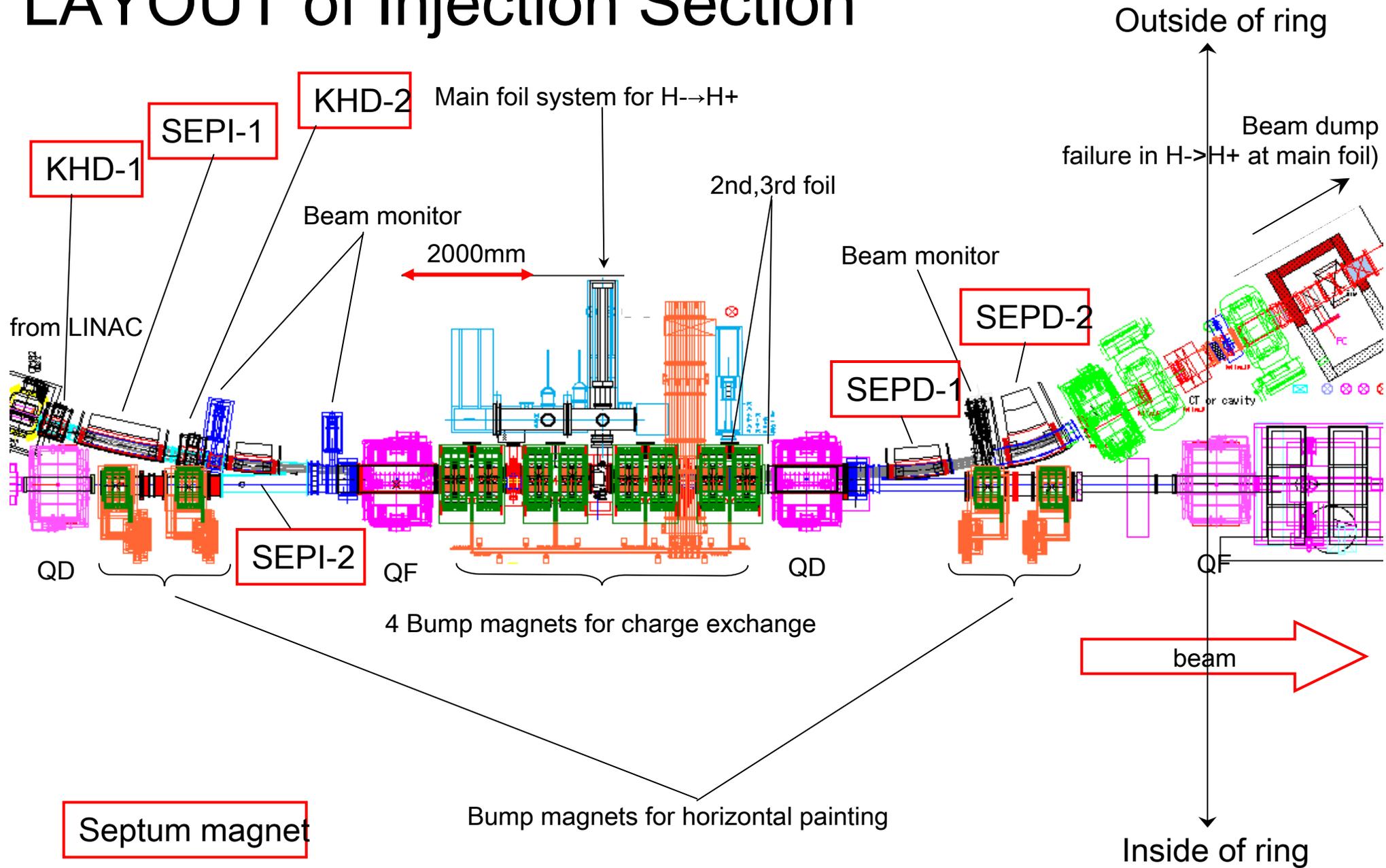
Bump magnets for painting

Fixed bump magnets

Bump magnets for painting



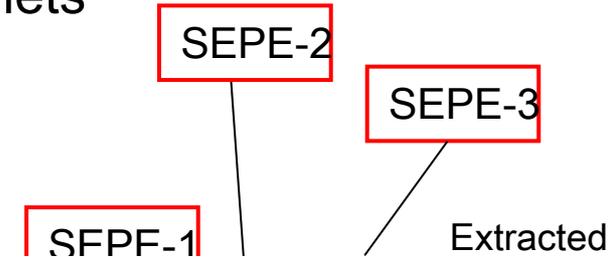
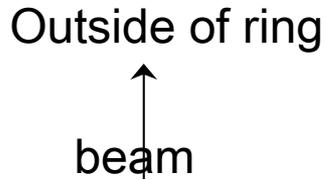
LAYOUT of Injection Section



EXTRACTION system

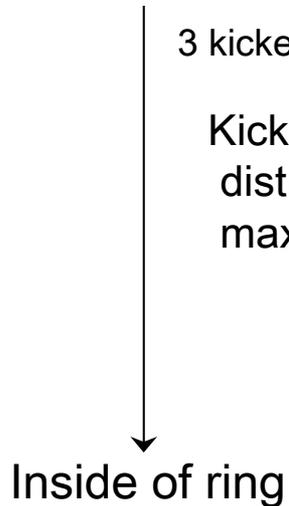
fast extraction = one turn extraction

8 kicker magnets and 3 septum magnets



3 kickers in vacuum tank 5 kickers in vacuum tank

Kickers
distributed type, matched 10 ohm
maximum voltage ~ 80kV



DESIGN of SEPTA

RCS = High Power Machine

- 1) Large aperture to allow the high intensity beam pass through with a low beam loss($\leq 0.1\%$).

aperture for injection beam 30 pimmrad
aperture for extraction beam 326 pimmrad - collimator aperture
- 2) Protection against the high radiation ($>100\text{MGy}/30\text{years}$ in septum coils).
- 3) High durability to avoid maintenance after high activation.

POLICY

Septum magnets are designed to operate in **DC excitation** current for mechanical stability and to use in low voltage to be easy to insulate.

Septum magnets are operated **in the air (out of the vacuum)**, to avoid an accident of cooling water leaking into the vacuum system of the ring.
(beam runs in vacuum duct)

DESIGN PARAMETERS of SEPTUM MAGNET

		Injection		Dump		Extraction			Injection
	unit	入射用 SEPI-1	入射用 SEPI-2	廃棄用 SEPD-1	廃棄用 SEPD-2	出射用 SEPE-1	出射用 SEPE-2	出射用 SEPE-3	可変偏向 KHD
number of magnets	台	1	1	1	1	1	1	1	2
particle		400Mev,H ⁺	400Mev,H ⁺	400Mev,H ⁺	400Mev,H ⁺	3GeV,H ⁺	3GeV,H ⁺	3GeV,H ⁺	400Mev,H ⁺
field strength	T	0.487	0.439	0.501	1.086	0.695	1.402	1.659	0.4195
effective length	mm	1400	800	1000	1000	900	1000	1000	300
gap width	mm	370	348	368	622	336	521	743	406
gap height	mm	136	136	136	140	223	189	166	160
wave form		DC							DC+AC(3%)
environment		大氣中(to operate in air, beam passing in vacuum duct in gap)							
min. septum thickness (duct+coil+shield)	mm	87	45	51	340	34	90	260	91
material of core		電磁軟鉄 JIS SUYP-1 (electromagnetic soft iron; solid)							0.5mm lamination
mass of core	kg	2515	1212	1724	12297	1751	7747	15004	485
magnetic attraction	tonf	3.69	1.67	2.92	21.84	2.28	31.6	57.2	0.71
excitation current	A	6246	5650	6787	5603	11176	12312	11035	1963
turn number of coils	turn	8	8	8	24	10	16	20	24
conductor size	mm ²	16*16-φ10 64*16-φ10	16*16-φ10 64*16-φ10	16*16-φ10 64*16-φ10	16*16-φ10 64*16-φ10	19*19-φ8 76*19-φ8	19*19-φ10 76*19-φ10	18*80-φ10	16*16-φ10
max. current density	A/mm ²	35.2	31.8	38.2	31.6	48.5	43.6	8.5	14
voltage of coil	V	20	14	19	53	33	28	17	22.3
electro-magnetic force	tonf	1.53	0.68	1.25	6.71	3.17	12.68	16.81	0.26
power loss in coil	kW	127	78	127	295	364	285	185	45
no.of cooling channel		8	8	8	24	20	16	20	24
cooling of coils		強制循環水直接水冷(water)							
flow rate	l/m	75	75	75	226	189	151	115	40
flow speed	m/s	2	2	2	2	2	2	1.2	2
pressure loss	kgf/cm ²	0.77	0.7	0.73	0.75	0.75	0.76	0.32	3.16
temp. rise	°C	24	18	24	19	28	27	23	17

How we determined parameters of coils?

Ex1) SEPI-1,2 SEPD-1,2 have same or near gap height...136,136,136,140mm

Allowed septum thickness of SEPI-1 and SEPD-1 are smallest in them.

We determined their parameters at first.

Allowed space for coil is about 16mm width.

It is need to reduce turn number,

to be low voltage, to be good mechanical stability, to be easy to fabricate...

Durability of coils has priority over the cost of power supplies and power feeds

So we determined number of row of coil to one, i.e. cc

Because square hollow conductor is to be easier to w
we determined height size of conductor to 16mm.

Turn number of coil = gap height / 16mm = 136 / 16 =

Other magnets use the same hollow conductor

because of to use the same parts of cooling channels

Ex2) SEPE-1,2,3

Turn number ratio is fixed to excite them in series

to use near square conductor in SEPE-1,2

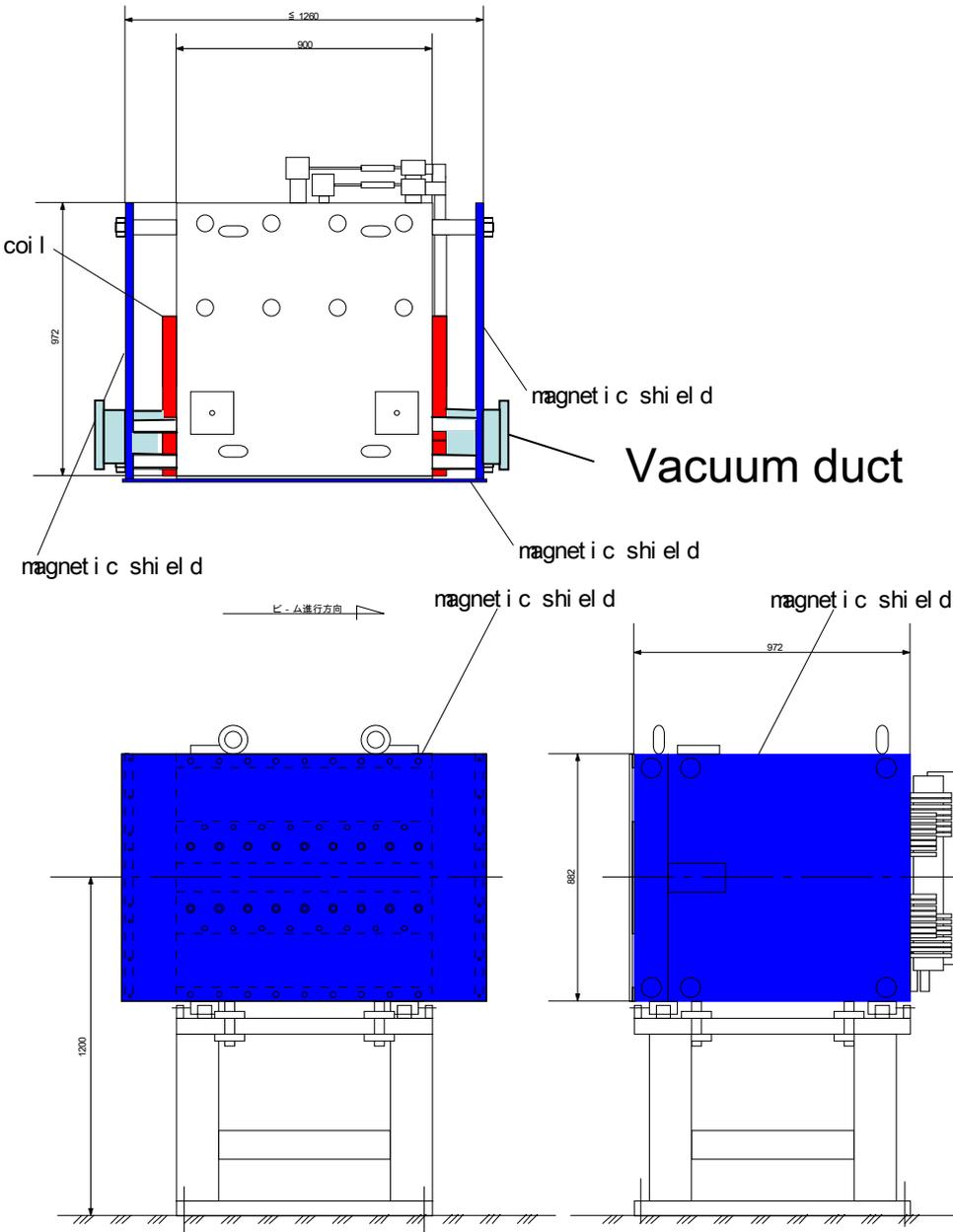
to reduce turn number

to reduce cost of power supplies

to reduce cost of power feed

limit of size of hollow conductor

We determined turn no. comprehensively.



A prototype magnet

gap height	142 mm
magnetic field in the gap	1.13 T
excitation current	12800 A
turn number of coil	10

Ceramic coating is used as the electronic insulation material due to its strength against high radiation ($>>100\text{MGy}$).

All cooling pipes are made of SUS304; **non-magnetic stainless steel(SUS304)** due to its hardness against erosion and corrosion by the flow of cooling water.

Titanium metal is used as the material of the vacuum duct in the gap because of its strength against activation.

Magnetic shield

Coil support

*注意：導体高はできる限り磁極間隙高に近づけることが重要で導体絶縁物厚と合わせて別途指示する

580

580

磁極間隙幅

127^{-0.5}+0.5

セプタム幅

202(参考値)

251(参考値)

Titanium duct

絶縁体スペース
可能なかぎり真空ダクト幅に振り向けること

EM force

EM force

142

100
磁極間隙高
≧90(参考値)
導体高*
指定値
±0.5

≧90(参考値)
導体高*

セプタム導体

戻導体

セプタム導体押板固定ボルト
M0-M6(参考)

セプタム導体押板
SUS304厚10mm(参考値)

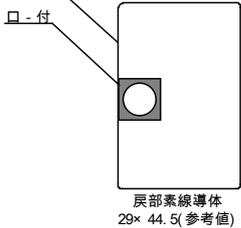


silver solder

Qi

SUS304 pipe (φ 10-φ 8)

セラミック溶射絶縁(0.2~0.3)



戻部素線導体
29×44.5(参考値)

ceramic coating 0.2~0.3mm thickness

CROSS SECTION OF GAP

Assembling coils

Cooling pipe (SUS304 stainless steel)
1 water channel / 1 turn $\phi 12$ - $\phi 10$

QuickTimey Ç²
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150



White parts are coated of ceramic, sprayed with melting ceramic, Total thickness is 0.2~ 0.3mm.

Ceramic coating

Engineers of the company of ceramic coating say

Best thickness is 0.2-0.3mm (10 X 0.02mm)

if less than this, electric insulation becomes uncertain.

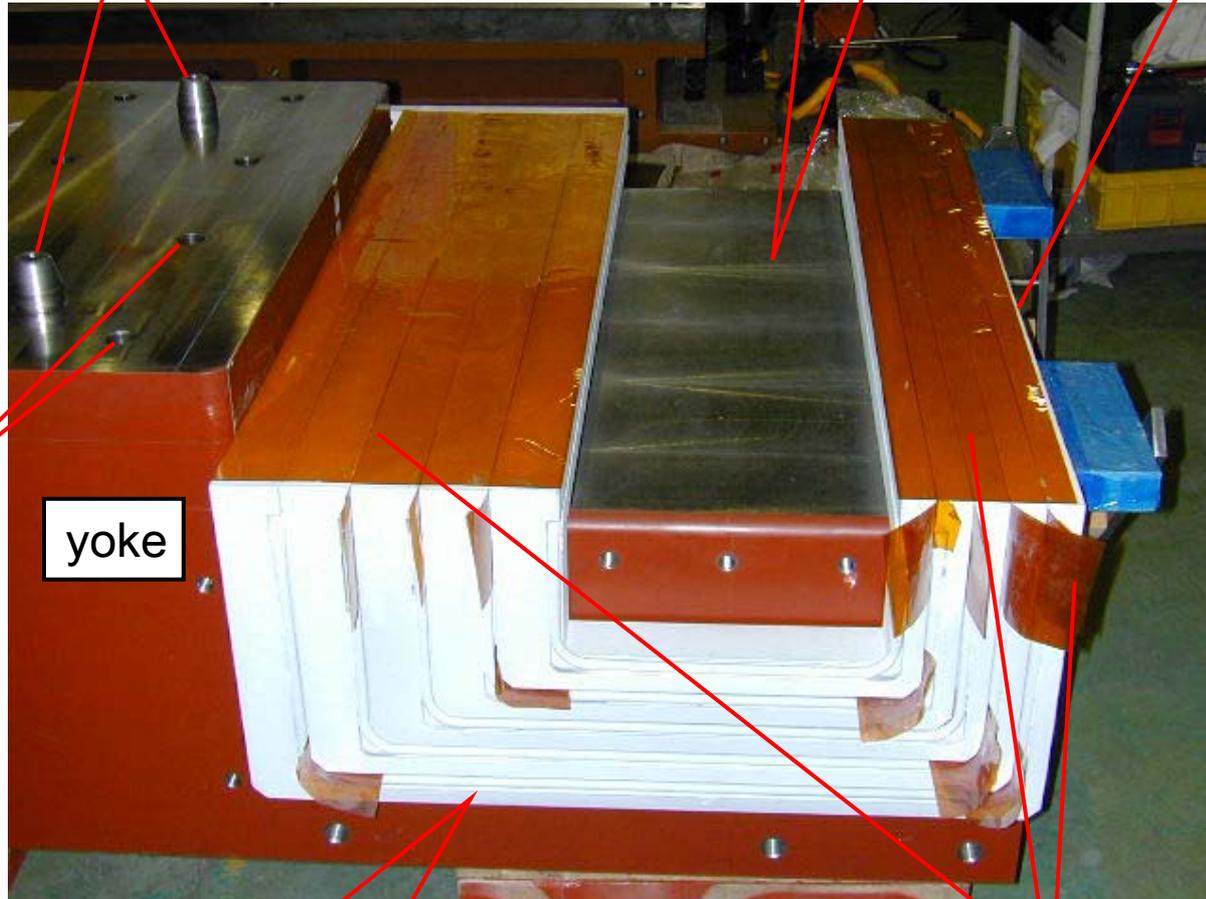
if more than this, coating becomes non-flexible, to be apt to crack.

Coils into iron core

Keys between up and down yoke

Gap surface

Medium plane



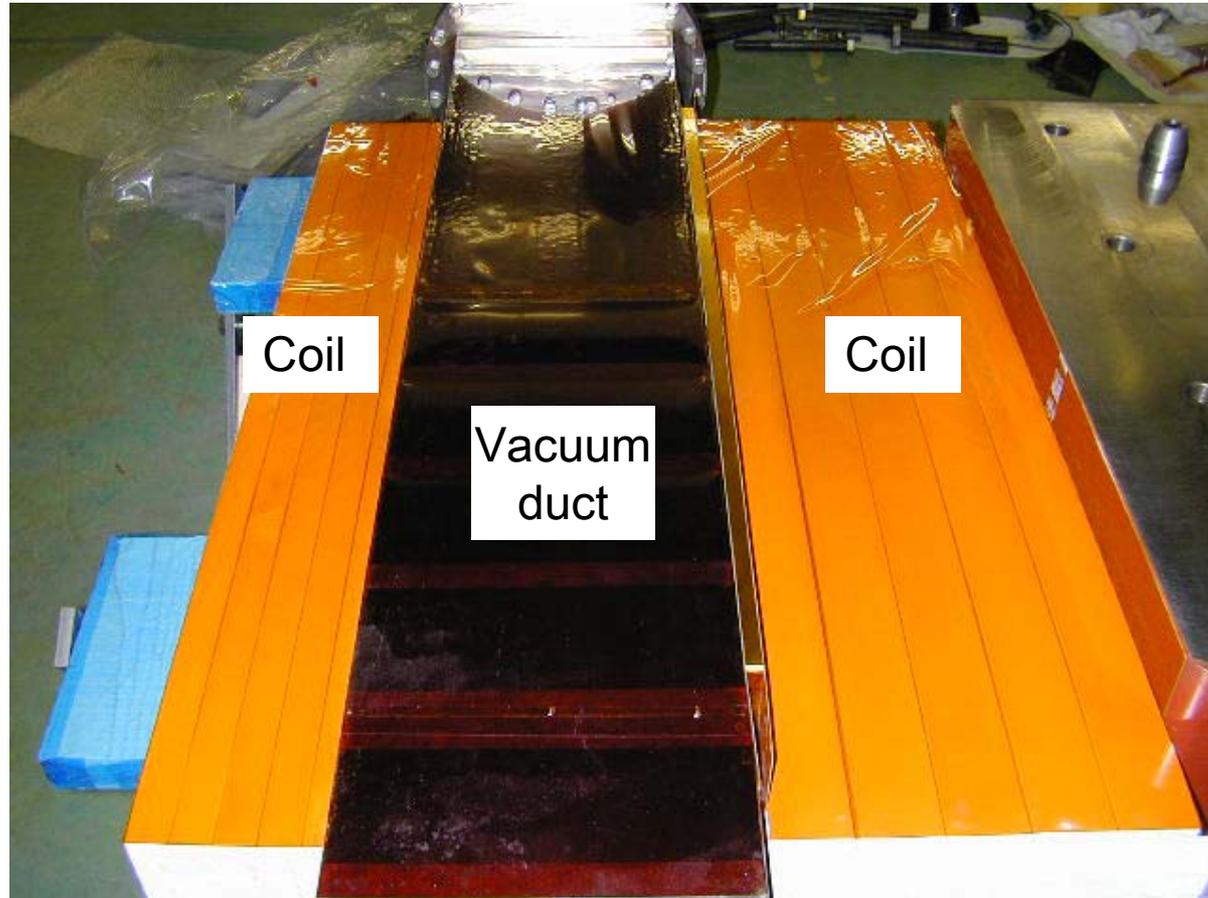
Volt holes

yoke

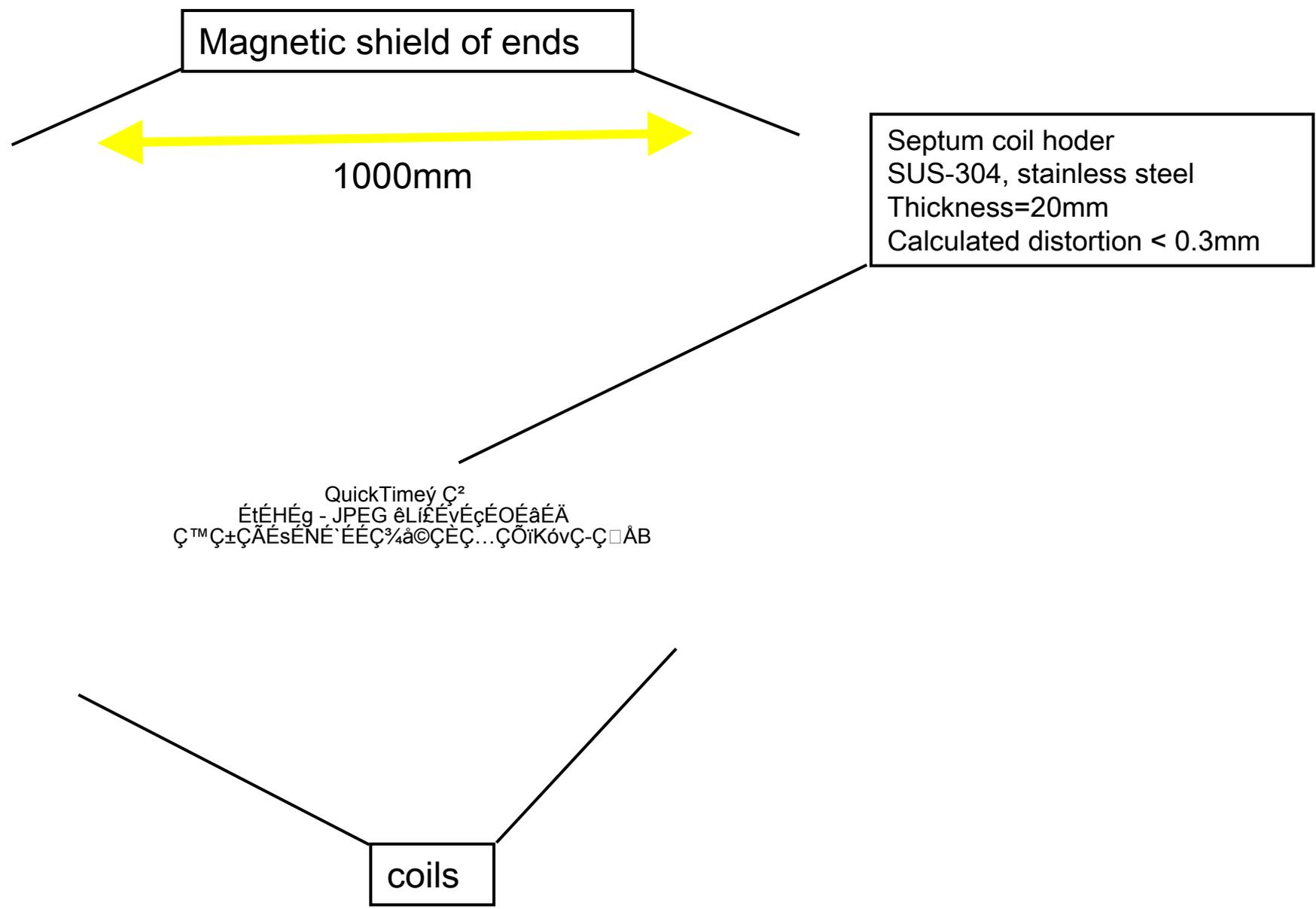
Half of coil assy.

We put KAPTON sheets in order to defend coating from breaking during assemble work.

Vacuum duct into magnet



End-shield and septum coil holder



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end view, removed magnetic shield



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End holder of coils

Concept of coil support and conductor insulation

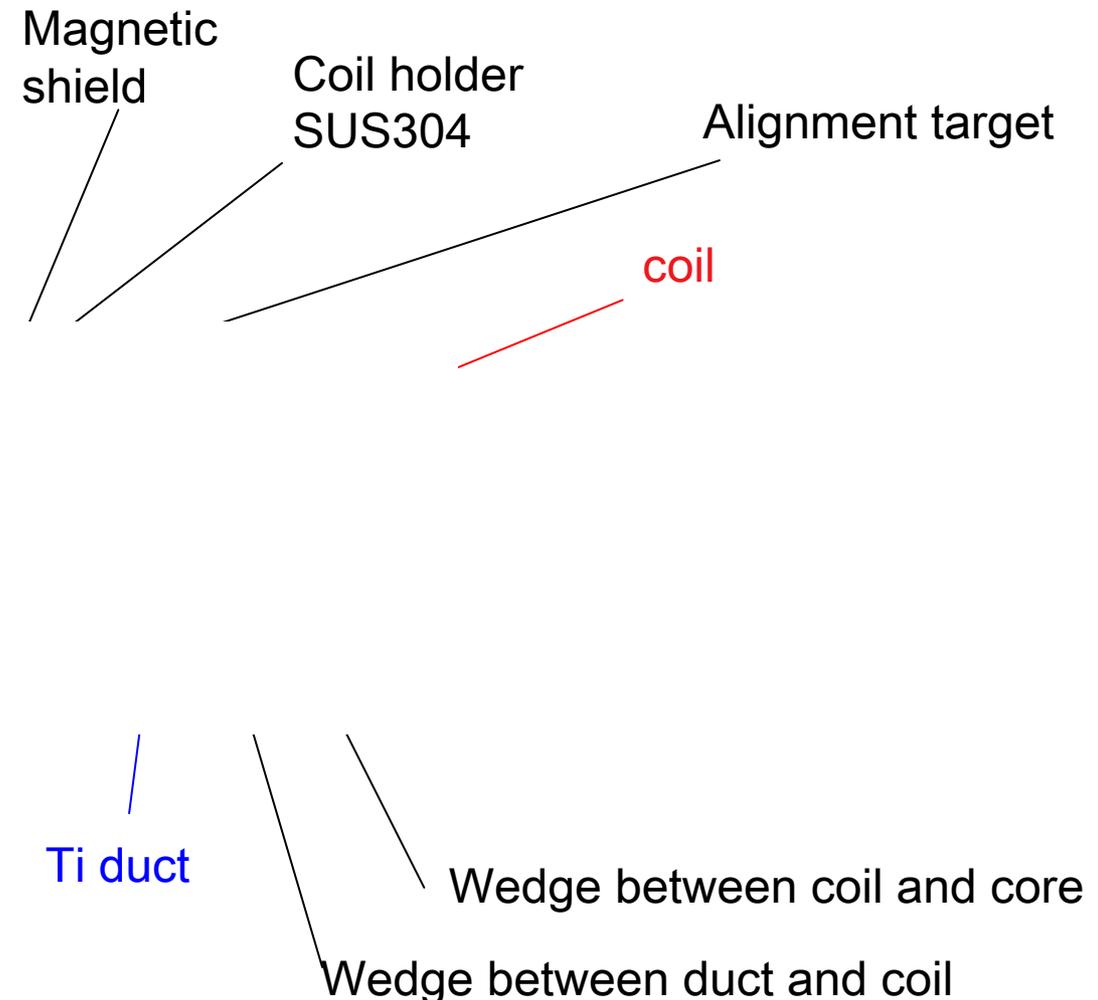
□ Coil supported by sandwiched between coil holder and duct.

Coil is only individually ceramic-coated to insulate.

Ground insulation is none.

We put KAPTON sheets around conductors in order to defend coating from breaking during assemble work.

We put soft metal, Al sheets between coils and duct,
Between coils and iron in order to slip conductors
As distorting by thermal force or electro-magnetic Force.



WaveForm of BUMP MAGNETS

